## Features

- FM Double-conversion System
- Integrated Second IF Filter with Software-controlled Bandwidth
- Completely Integrated FM Demodulator
- Soft Mute and Multipath Noise Cancellation
- Receiving Condition Analyzer
- AM Up/Down-conversion System
- AM Preamplifier with AGC and Stereo Capability
- 3-wire Bus Controlled
- Search Stop Signal Generation (AM and FM)
- Automatic Alignment Possible
- Pin Compatible with ATR4255
- World Tuner, US Weatherboard, J-band
- Lead-free Package

Electrostatic sensitive device. Observe precautions for handling.


## Description

The ATR4258 is a highly integrated AM/FM front-end circuit manufactured using Atmel's advanced BICMOS technology. It represents a complete, automatically adjustable AM/FM front end, containing a double-conversion system for FM and an up/down-conversion receiver for AM with IF1 $=10.7 \mathrm{MHz}$ and IF2 $=450 \mathrm{kHz}$. The front end is suitable for digital or analog AF-signal processing. Together with the PLL U4256BM, an automatically aligned high-performance AM/FM tuner can be built. These ICs are dedicated for highly sophisticated car radio applications.

Figure 1. Block Diagram


## Pin Configuration

Figure 2. Pinning SSO44


## Pin Description

| Pin | Symbol | Function |
| :---: | :---: | :---: |
| 1 | MX1FMA | $1^{\text {st }}$ mixer FM input A |
| 2 | MX1FMB | $1{ }^{\text {st }}$ mixer FM input B |
| 3 | MX1AMB | $1{ }^{\text {st }}$ mixer AM input B |
| 4 | GNDMX | Ground $1^{\text {st }}$ mixer, preamplifier AGC |
| 5 | FMAGC | FM preamplifier AGC |
| 6 | AMVREG | AM control voltage |
| 7 | AMAGC | AM preamplifier AGC |
| 8 | AMPLPF | AM AGC LP filter |
| 9 | METER | Field strength output |
| 10 | ADJAC | Adjacent channel detection output |
| 11 | MPX | Multiplex signal |
| 12 | V57 | 5.7 V reference voltage |
| 13 | OSCB | Oscillator basis |
| 14 | OSCE | Oscillator emitter |
| 15 | GNDOSC | Oscillator ground |
| 16 | OSCOUT | Oscillator output |
| 17 | EN | 3-wire bus enable |
| 18 | CLK | 3-wire bus clock |
| 19 | DATA | 3-wire bus data |
| 20 | IF2OUT | $2^{\text {nd }}$ IF amplifier output |
| 21 | INT | Interrupt, stop signal |
| 22 | MX2LO | 10.25 MHz input for $2^{\text {nd }}$ mixer |
| 23 | MX2OB | $2{ }^{\text {nd }}$ mixer output B |
| 24 | MX2OA | $2^{\text {nd }}$ mixer output A |
| 25 | GND | Ground |
| 26 | MX2IN | $2^{\text {nd }}$ mixer input |
| 27 | V3P | 3 V reference for AMPIN, AMIFAGC, Control, IF2IN |
| 28 | IF2IN | $2^{\text {nd }}$ IF amplifier input |
| 29 | V3 | 3 V reference for IF1OUT, MX2IN |
| 30 | IF1OUT | $1^{\text {st }}$ IF amplifier output |
| 31 | DEV | Deviation detect output, test output |
| 32 | OPLPF | Operating point LPF |
| 33 | IF1AMI | $1{ }^{\text {st }}$ IF AM amplifier input |
| 34 | SMUTE | Soft MUTE control input |
| 35 | IFAGCH | IF AGC LP filter high time |
| 36 | IFAGCL | IF AGC LP filter low time constant |
| 37 | FILADJ | Filter adjust |
| 38 | IF1FMI | $1^{\text {st }}$ IF FM amplifier input |
| 39 | IF1REF | $1{ }^{\text {st }}$ IF \& MX1OUT reference, MX1AM A, MX1AM B |
| 40 | MULTIP | Multipath detection output |
| 41 | MX1AMA | $1{ }^{\text {st }}$ mixer AM input A |
| 42 | VS | Supply voltage |
| 43 | MX1OA | $1{ }^{\text {st }}$ mixer output A |
| 44 | MX1OB | $1{ }^{\text {st }}$ mixer output B |

## 4

## Functional Description

## Reception Mode

The ATR4258 implements an AM up/down-conversion reception path from the RF input signal to the AM-demodulated audio frequency output signal, and for FM/WB reception a double-conversion reception path from the RF input signal to the FM-demodulated multiplex signal (MPX). A VCO and an LO prescaler for AM are integrated to generate the LO frequency for the $1^{\text {st }}$ mixer. Automatic gain control (AGC) circuits are implemented to control the preamplifier and IF stages in the AM and FM reception path.
For improved FM performance, an integrated IF filter with adjustable bandwidth, a softmute feature and an automatic multipath noise cancellation (MNC) circuit are fully integrated. A powerful set of sensors is provided for receiving condition analysis and stop signal generation.
Several register bits (bit 0 to bit 93) are used to control circuit operation and to adapt certain circuit parameters to the specific application. The control bits are organized in two 8 -bit and three 24 -bit registers that can be programmed by the 3 -wire bus protocol. The bus protocol and the bit-to-register mapping is described in the section " 3 -wire Bus Description" on page 20. The meaning of the control bits is mentioned in the following sections.
The integrated VCO has a high frequency range. Additionally the VCO has a special VCO divider which allows (in connection with the VCO) the reception of all analog world bands.

The IC can be operated in four different modes. Mode AM, FM, WB, and Standby are selected by means of bit 92 and bit 93 according to Table 1 on page 6.

Additionally to the operating modes, the signal paths can be set separately. Bit 62 selects the first mixer and AGC, bit 63 selects the $1^{\text {st }}$ amplifier stage. The recommended settings of bit 62 and bit 63 are included in Table 1 on page 6.
In AM mode the AM mixer, the AM RF-AGC and the $1^{\text {st }}$ IF AM amplifier at pin 33 are activated. The input of the $2^{\text {nd }}$ IF amplifier is connected to pin 28 and the output of the $2^{\text {nd }}$ IF amplifier is fed to the AM demodulator. The output of the AM demodulator is available at MPX output pin 11.
In FM mode the FM mixer, the FM RF-AGC and the $1^{\text {st }}$ IF FM amplifier at pin 38 are activated. The bandwidth of the output tank at pin 23, pin 24 is increased and the input of the $2^{\text {nd }}$ IF amplifier can be switched between pin 23 and pin 24 and pin 28 . The output of the $2^{\text {nd }}$ IF amplifier is fed to the integrated band filter and FM demodulator. The output of the FM demodulator is available at MPX output pin 11.

The WB mode is similar to the FM mode, but to reduce the bandwidth the AM IF amplifier with the AM filter (bit $63=1$ ) can be used. In WB mode the range of the integrated filter bandwidth control is shifted to lower bandwidth and the gain of the FM demodulator is increased.
In standby mode the mixers, IF amplifiers and AGC circuits are deactivated to reduce current consumption.

Table 1. Operating Mode

| AM/FM/Weather Channel | Bit 93 | Bit 92 | Bit 63 | Bit 62 |
| :---: | :---: | :---: | :---: | :---: |
| Standby | 0 | 0 | X | X |
| FM | 0 | 1 | 0 | 0 |
| AM | 1 | 0 | 1 | 1 |
| Weather band | 1 | 1 | 1 | 0 |

## Test Mode

## VCO/Local Oscillator Prescaler

A special test mode is implemented for final production test only. This mode is activated by setting bit $9=1$. This mode is not intended to be used in customer applications. For normal operation, bit 9 has to be set to 0 . Bit 22 to bit 30 are deactivated in normal operation mode.

Table 2. Test Mode

| Mode | Bit 9 |
| :---: | :---: |
| Normal operation | 0 |
| Test mode | 1 |

An oscillator circuit is implemented to build a VCO as proposed in the application schematic. The VCO frequency is used to generate the LO frequency of the $1^{\text {st }}$ mixer stages. The control voltage of the VCO is usually generated by the PLL circuit U4256BM. The VCO frequency has a range of 70 MHZ to 250 MHz to allow the reception of all analog world bands.

A main element of the implemented oscillator circuit is a bipolar NPN transistor. The internally biased base is connected to pin 13 and the emitter to pin 14. An AGC circuit (bit 30) can be activated to increase the emitter current until the appropriate oscillation level is reached. The fundamental emitter current can be changed by bit 52 .

Table 3. Local Oscillator AGC

| Local Oscillator (VCO) | Bit 30 |
| :--- | :--- |
| AGC off (default) | 0 |
| AGC on | 1 |

Table 4. Local Oscillator Gain

| Local Oscillator (VCO) | Bit 52 |
| :--- | :--- |
| Low Gain | 0 |
| High Gain | 1 |

In addition (to the AM prescaler) a special VCO prescaler is implemented for all modes (AM, WB and FM). The divider factor of the prescaler buffer provides the signal of the buffered output (at pin 16) and the prescaler VCO provides the signal of the $1^{\text {st }} \mathrm{FM}$ mixer stage and AM prescaler. Examples of VCO prescaler settings are described in section "Application Information" on page 29.

The divider factor of the VCO and buffer prescaler can be selected according Table 5 on page 7.

Table 5. Local Oscillator Prescaler (VCO/Buffer Divider)

| Prescaler VCO | Prescaler Buffer | Bit 12 | Bit 11 | Bit 10 |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | X | 0 | 0 |
| 1.5 | 3 | 0 | 0 | 1 |
| 1.5 | 1.5 | 1 | 0 | 1 |
| 2 | 2 | $X$ | 1 | 0 |
| 3 | 3 | $X$ | 1 | 1 |

Note: The U4256 FMOSCIN (pin 19) input frequency is limited to 160 MHz .
The FM RF-AGC circuit includes a wide-band level detector at the input pin 1 of the FM mixer and an in-band level detector at the output of the FM IF amplifier (pin 30). The outputs of these level detectors are used to control the current into the pin diode (see Figure 3) in order to limit the signal level at the FM mixer input and the following stages. The maximum pin diode current is determined by R115 and the time constant of the AGC control loop can be adjusted by changing the value of C111.

The AGC threshold level at the input of the FM mixer can be adjusted by bit 64 and bit 65 according to Table 6. The in-band AGC threshold refers to the FM mixer input (pin 1, pin 2) depends on the gain of the FM IF amplifier and can be adjusted by bit 89 to bit 91 .

Table 6. FM-AGC Threshold

| FM-AGC Threshold | Bit 65 | Bit 64 |
| :---: | :---: | :---: |
| $100 \mathrm{~dB} \mu \mathrm{~V}$ | 0 | 0 |
| $97 \mathrm{~dB} \mu \mathrm{~V}$ | 0 | 1 |
| $94 \mathrm{~dB} \mu \mathrm{~V}$ | 1 | 0 |
| $91 \mathrm{~dB} \mu \mathrm{~V}$ | 1 | 1 |

Figure 3. FM RF-AGC Bit 92


AM RF-AGC

FM $1^{\text {st }}$ Mixer

AM $1^{\text {st }}$ Mixer

The AM RF-AGC controls the current into the AM pin diodes (pin 7) and the source drain voltage of the MOSFET in the AM preamplifier stage (pin 6) to limit the level at the AM mixer input (pin 3, pin 41). This threshold level can be set by bit 64 and bit 65 . If the level at the AM mixer input exceeds the selected threshold, the current into the AM pin diodes is increased. If this step is not sufficient, the source drain voltage of the MOSFET is decreased. The time constant of the AGC control loop can be adjusted by changing the value of the capacitor at pin 8 .

Table 7. AM-AGC Threshold

| AM-AGC Threshold | Bit 65 | Bit 64 |
| :---: | :---: | :---: |
| $91 \mathrm{~dB} \mu \mathrm{~V}$ | 0 | 0 |
| $94 \mathrm{~dB} \mu \mathrm{~V}$ | 0 | 1 |
| $97 \mathrm{~dB} \mu \mathrm{~V}$ | 1 | 0 |
| $100 \mathrm{~dB} \mu \mathrm{~V}$ | 1 | 1 |

In the $1^{\text {st }} \mathrm{FM}$ mixer stage, the FM reception frequency is down converted to the $1^{\text {st }} \mathrm{IF}$ frequency. The VCO frequency is used as LO frequency for the mixer.

The AM $1^{\text {st }}$ mixer is used for up-conversion of the AM reception frequency to the $1^{\text {st }} \mathrm{IF}$ frequency. Therefore, an AM prescaler is implemented to generate the necessary LO frequency from the VCO frequency. The divide factor of the AM prescaler can be selected according to Table 8. (The AM prescaler is only active in AM mode).

Table 8. Divide Factor of the AM Prescaler

| Divider (AM Prescaler) | Bit 93 | Bit 92 | Bit 84 | Bit 83 | Bit 82 | Bit 81 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Divide by 2 | 1 | 0 | 0 | 0 | 0 | 0 |
| Divide by 3 | 1 | 0 | 0 | 0 | 0 | 1 |
| Divide by 4 | 1 | 0 | 0 | 0 | 1 | 0 |
| Divide by 5 | 1 | 0 | 0 | 0 | 1 | 1 |
| Divide by 6 | 1 | 0 | 0 | 1 | 0 | 0 |
| Divide by 7 | 1 | 0 | 0 | 1 | 0 | 1 |
| Divide by 8 | 1 | 0 | 0 | 1 | 1 | 0 |
| Divide by 9 | 1 | 0 | 0 | 1 | 1 | 1 |
| Divide by 10 | 1 | 0 | 1 | $X$ | $X$ | $X$ |

## FM $1^{\text {st }}$ IF Amplifier

AM $1^{\text {st }}$ IF Amplifier
$2^{\text {nd }}$ Mixer

A programmable gain amplifier is used in FM (and WB) mode between pin 38 and pin 30 to compensate the loss in the external ceramic band filters. The gain of this amplifier is adjusted by bit 89 to bit 91 . The input and the output resistance is $330 \Omega$ and fits to external ceramic filters.

Two different temperature coefficients of the FM IF amplifier can be selected by bit 66 .

Table 9. Gain of the FM IF Amplifier

| Gain FM IF | Bit 91 | Bit 90 | Bit 89 |
| :---: | :---: | :---: | :---: |
| 19 dB | 0 | 0 | 0 |
| 21 dB | 0 | 0 | 1 |
| 23 dB | 0 | 1 | 0 |
| 25 dB | 0 | 1 | 1 |
| 27 dB | 1 | 0 | 0 |
| 28 dB | 1 | 0 | 1 |
| 29 dB | 1 | 1 | 0 |
| 30 dB | 1 | 1 | 1 |

Table 10. Temperature Coefficient Setting of FM IF Amplifier

| Temperature Coefficient (TC) of the IF Amplifier | Bit 66 |
| :---: | :---: |
| $\mathrm{TK}_{\min }$ (TK 1) | 0 |
| $\mathrm{TK}_{\max }$ (TK 2) | 1 |

In AM and WB mode, the gain of the $1^{\text {st }}$ IF amplifier is controlled by the IF-AGC to extend the control range of the IF-AGC.

The $2^{\text {nd }}$ mixer is used in AM, FM and WB mode. The mixer input has $330 \Omega$ input resistance and can be connected directly to an external ceramic filter.
In FM mode, the high output resistance of the second mixer is reduced to increase the bandwidth of the tank at the mixer output. The output resistance can be selected by bit 60 and bit 61.
In AM and WB mode bit 61 and bit 62 should be set to 0 .

Table 11. $2^{\text {nd }}$ Mixer Output Resistance in FM Mode

| Bit 61 | Bit 60 | Output Resistance (Bit 54 = 0) | Output Resistance (Bit 54 = 1) |
| :---: | :---: | :---: | :---: |
| 0 | 0 | $3.3 \mathrm{k} \Omega$ | $\sim 100 \mathrm{k} \Omega$ |
| 0 | 1 | $0.63 \mathrm{k} \Omega$ | $0.78 \mathrm{k} \Omega$ |
| 1 | 0 | $0.47 \mathrm{k} \Omega$ | $0.55 \mathrm{k} \Omega$ |
| 1 | 1 | $0.29 \mathrm{k} \Omega$ | $0.32 \mathrm{k} \Omega$ |

The LO frequency of the $2^{\text {nd }}$ mixer ( 10.25 MHz ) has to be applied at pin 22. This signal is usually generated by the PLL circuit U4256BM.

Table 12. FM Bandwidth Mixer 2

| Bit 61 | Bit 60 | FM Bandwidth Mixer 2 |
| :---: | :---: | :---: |
| 0 | 0 | 150 kHz |
| 0 | 1 | 200 kHz |
| 1 | 0 | 250 kHz |
| 1 | 1 | 450 kHz |

Note: $\quad$ The bandwidth is also dependant on the values of the application circuit.
$2^{\text {nd }}$ IF Amplifier

IF-AGC

In AM and WB mode, the input of the second IF amplifier is pin 28, is externally connected to the $2^{\text {nd }}$ mixer tank through the AM ceramic filter to achieve channel selectivity. During normal FM operation (bit $54=0$ ), the input of the second IF amplifier is connected to the $2^{\text {nd }}$ mixer output (pin 23, pin 24) and the integrated FM band filter is used for channel selectivity only. It is possible to use an additional external filter between the $2^{\text {nd }}$ mixer tank and pin 28 in FM mode by setting bit 54 to 1 .

Table 13. $2^{\text {nd }}$ IF Filter in FM Mode

| 2nd IF Filter | Bit 54 |
| :---: | :---: |
| Internal filter | 0 |
| External and internal filter | 1 |

The IF-AGC controls the level of the $2^{\text {nd }}$ IF signal that is passed to the AM demodulator input or the integrated FM band filter and to the $2^{\text {nd }}$ IF output, pin 20.

Two different time constants of the IF-AGC can be selected by the capacitors at pin 35 (IFAGCH) and pin 36 (IFAGCL). The short time constant (IFAGCL) is used in FM/WB mode and in AM search mode. The long time constant (IFAGCH) is used for AM reception.

Table 14. IF-AGC Time Constant

| Mode | Bit 92 | Bit 88 | IF AGC Time Constant |
| :---: | :---: | :---: | :---: |
| FM/WB | 1 | X | IFAGCL (fast) |
| AM reception | 0 | 0 | IFAGCH (slow) |
| AM search | 0 | 1 | IFAGCL (fast) |

In FM/WB mode, the output signal of the FM demodulator is applied to pin 35 via a series resistor of about $95 \mathrm{k} \Omega$ This low-pass filtered output signal of the FM demodulator is used for the FM demodulator fine adjustment, for muting and as a reference for the deviation sensor.

## $2^{\text {nd }}$ IF Output

## Automatic IF Center Frequency Adjustment

The $2^{\text {nd }}$ IF after the gain-controlled $2^{\text {nd }}$ IF amplifier is available at pin 20 (bit $55=0$ ). In AM mode, this signal may be used for an external AM stereo decoder. Alternatively, a signal corresponding to the logarithmic field strength after the integrated FM band filter, which is used for multipath detection, can be switched to pin 20 by setting bit $55=1$.

Table 15. Pin 20 Output Setting

| Pin 20 | Bit 55 |
| :---: | :---: |
| $2^{\text {nd }}$ IF output | 0 |
| Multipath field strength | 1 |

Integrated active filters are used in the FM band filter, FM demodulator and adjacent channel sensor. The center frequency of these filters is automatically adjusted to the second IF frequency of 450 kHz . The frequency of 10.25 MHz at pin 22 is used as a reference for this alignment.

Figure 4. Automatic IF Center Frequency Adjustment


For fine tuning, the center frequency of all these integrated active filters (band filter and demodulator) can be shifted in steps of 6.25 kHz by means of bit 56 to bit 59. Additionally, the center frequency of the band filter can be adjusted separately by means of bit 14 to bit 17.

Table 16. $2^{\text {nd }}$ IF Center Frequency

| IF Center | Bit 59 | Bit 58 | Bit 57 | Bit 56 |
| :---: | :---: | :---: | :---: | :---: |
| 450.00 kHz | 0 | 0 | 0 | 0 |
| 456.25 kHz | 0 | 0 | 0 | 1 |
| 462.50 kHz | 0 | 0 | 1 | 0 |
| 468.75 kHz | 0 | 0 | 1 | 1 |
| 475.00 kHz | 0 | 1 | 0 | 0 |
| 481.25 kHz | 0 | 1 | 0 | 1 |
| 487.50 kHz | 0 | 1 | 1 | 0 |
| 493.75 kHz | 0 | 1 | 1 | 1 |
| 450.00 kHz | 1 | 0 | 0 | 0 |
| 443.75 kHz | 1 | 0 | 0 | 1 |
| 437.50 kHz | 1 | 0 | 1 | 0 |
| 431.25 kHz | 1 | 0 | 1 | 1 |
| 425.00 kHz | 1 | 1 | 0 | 0 |
| 418.75 kHz | 1 | 1 | 0 | 1 |
| 412.50 kHz | 1 | 1 | 1 | 0 |
| 406.25 kHz | 1 | 1 | 1 | 1 |

Table 17. FM Band Filter Center Frequency Correction

| IF Correction | Bit 17 | Bit 16 | Bit 15 | Bit 14 |
| :---: | :---: | :---: | :---: | :---: |
| -0 kHz | 0 | 0 | 0 | 0 |
| -6.25 kHz | 0 | 0 | 0 | 1 |
| -12.50 kHz | 0 | 0 | 1 | 0 |
| -18.75 kHz | 0 | 0 | 1 | 1 |
| -25.00 kHz | 0 | 1 | 0 | 0 |
| -31.25 kHz | 0 | 1 | 0 | 1 |
| -37.50 kHz | 0 | 1 | 1 | 0 |
| -43.75 kHz | 0 | 1 | 1 | 1 |
| $+0 \mathrm{kHz}(\mathrm{default})$ | 1 | 0 | 0 | 0 |
| +6.25 kHz | 1 | 0 | 0 | 1 |
| +12.50 kHz | 1 | 0 | 1 | 0 |
| +18.75 kHz | 1 | 0 | 1 | 1 |
| +25.00 kHz | 1 | 1 | 0 | 0 |
| +31.25 kHz | 1 | 1 | 0 | 1 |
| +37.50 kHz | 1 | 1 | 1 | 0 |
| +43.75 kHz | 1 | 1 | 1 | 1 |

Integrated FM Band Filter For FM reception a band filter with variable bandwidth is integrated in front of the demodulator to provide channel selectivity on the $2^{\text {nd }} \mathrm{IF}$. The bandwidth of this filter can be adjusted by bit 0 to 3 (see Table 18) to be suitable for the present receiving condition. In WB mode, the bandwidth of the integrated filter is shifted to lower bandwidth values, while the necessary channel selectivity is achieved by an external ceramic filter.

The center frequency of the integrated FM band filter can be adjusted by means of bit 14 to 17 . The field strength after the integrated FM band filter that is available at pin 20 (bit $55=1$ ) can be used for this purpose.

Table 18. Bandwidth of the Integrated Band Filter

| IF Bandwidth FM | IF Bandwidth WB | Bit 3 | Bit 2 | Bit 1 | Bit 0 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 220 | 195 | 0 | 0 | 0 | 0 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| 200 | 160 | 0 | 0 | 1 | 1 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| 165 | 120 | 0 | 1 | 1 | 0 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| 130 | 80 | 1 | 0 | 0 | 1 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| 70 | - | 1 | 1 | 0 | 1 |
| 60 | - | 1 | 1 | 1 | 0 |
|  |  | 1 | 1 | 1 | 1 |

FM Demodulator
For weather band reception, the gain of the FM demodulator is increased and can be adjusted by means of bit 71 and bit 72 in order to increase the output voltage to compensate the low frequency deviation in weather band.
An integrated demodulator fine adjustment allows automatic fine tuning of the demodulator center frequency to the average frequency of the received signal. This feature is implemented for use in weather band mode and can be activated by setting bit 53 to 0 .

Figure 5. FM Demodulator Automatic Fine Tuning


The center frequency of the FM demodulator can be adjusted by means of bit 56 to 59 . At the center frequency, the DC voltage at the MPX output pin 11 is equal to the MPX offset voltage that can be measured at pin 11 while MPX mute is active (bit $7=1$ ). This adjustment will affect the center frequency of all integrated filters as mentioned before.

Table 19. Demodulator Gain in Weather Band Mode

| Demodulator Gain in Weather Band Mode Relative to FM Mode | Bit 72 | Bit 71 |
| :---: | :---: | :---: |
| 14 dB | 0 | 0 |
| 17 dB | 0 | 1 |
| 21 dB | 1 | 0 |
| 23 dB | 1 | 1 |

Table 20. Demodulator Fine Adjustment

| Demodulator Fine Adjustment | Bit 53 |
| :---: | :---: |
| Fine tuning ON | 0 |
| Fine tuning OFF | 1 |

## Soft Mute

The soft mute functionality is implemented to reduce the output level of the FM demodulator at low input signal levels to limit the noise at the MPX output in this case. If the input level falls below an adjustable threshold continuously, the output of the FM demodulator is continuously muted with decreasing input level until a maximum mute value is reached. The threshold for the start of soft mute and the maximum mute can be adjusted. The signal level for 3 dB mute can be set by means of bit 68 to bit 70 and the maximum value for soft mute can be selected by bit 67 . The steepness and the time constant of the soft mute can be adjusted by the resistor and capacitor between pin 34 and pin 29.

The field strength signal available at pin 9 is used for soft mute. Therefore, the soft mute threshold that referred to the input of the FM mixer depends on the gain from the FM mixer input to the field strength sensor and on the setting of field strength offset (bit 15 to bit 21).

Table 21. Soft Mute Threshold

| Relative Soft Mute Threshold | Bit 70 | Bit 69 | Bit 68 |
| :---: | :---: | :---: | :---: |
| Soft mute OFF | 0 | 0 | 0 |
| -18 dB | 0 | 0 | 1 |
| -15 dB | 0 | 1 | 0 |
| -12 dB | 0 | 1 | 1 |
| -9 dB | 1 | 0 | 0 |
| -6 dB | 1 | 0 | 1 |
| -3 dB | 1 | 1 | 0 |
| 0 dB | 1 | 1 | 1 |

Table 22. Maximum Soft Mute

| Maximum Value of Soft Mute | Bit 67 |
| :---: | :---: |
| 30 dB | 0 |
| 26 dB | 1 |

Figure 6. Soft Mute


## MPX Output

The output of the AM demodulator (AM mode) or the output of the FM demodulator (FM/WB mode) are available at the MPX output (pin 11).

The MPX output signal can be muted by setting bit 7 to 1 .
The bandwidth of the low-pass filter at the MPX output can be set by means of bit 79 to 90 kHz or 180 kHz .

Table 23. MPX Output Mute

| MPX Output | Bit 7 |
| :---: | :---: |
| MPX out, pin 11 normal operation | 0 |
| Mute ON | 1 |

Table 24. MPX Output Bandwidth

| Bandwidth MPX Low-pass Filter | Bit 79 |
| :---: | :---: |
| 90 kHz | 0 |
| 180 kHz | 1 |

Receiving Condition Analyzer

The ATR4258 implements several sensors that provide information about the receiving condition of the selected station.

Field Strength Sensor

## Field Strength Selection

The field strength sensor provides a DC voltage at pin 9 which represents the logarithmic field strength of the signal in the reception band.

The field strength information can be retrieved either from a level detector at the input of the $2^{\text {nd }}$ mixer (pin 26) or from the IF-AGC depending on the setting of bit 80 . The bandwidth of the field strength detection in the AGC is smaller than by using the level detector because of additional selectivity between the $2^{\text {nd }}$ mixer and the $2^{\text {nd }}$ IF amplifier particularly in AM and WB, but the field strength detection in the AGC is limited to the IF AGC range. Usually the field strength from the level detector is used in FM/WB mode and the AGC field strength is used in AM mode.

The field strength output at pin 9 can be adjusted by the bits 18 to 21 in 0.5 dB steps. This offset also has an influence on the soft mute levels.

Table 25. Field Strength Offset

| Offset Field Strength | Bit 21 | Bit 20 | Bit 19 | Bit 18 |
| :--- | :---: | :---: | :---: | :---: |
| 0.0 dB | 0 | 0 | 0 | 0 |
| 0.5 dB | 0 | 0 | 0 | 1 |
| 1.0 dB | 0 | 0 | 1 | 0 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| 7.5 dB | 1 | 1 | 1 | 1 |

Bit 80 and bit 13 allows the switches between narrow-band field strength and wide-band field strength information.

Table 26. Field Strength (Combined)

| Field Strength (Pin 9) Narrow-band/Wide-band | Bit 80 | Bit 13 |
| :--- | :---: | :---: |
| FM field strength (wide band) | 0 | 0 |
| Multipath field strength and FM field strength (wide band) | 0 | 1 |
| AM AGC field strength (narrow band) | 1 | 0 |
| Multipath field strength and AM AGC field strength (narrow band) | 1 | 1 |

## Search Stop Detector

A search stop detector is available in AM and FM/WB mode. A STOP condition is signaled (with a low level at pin 21) if the frequency of the IF signal is within a window around the center frequency of 450 kHz . The width of this search stop window can be set by bit 85 to bit 87 in the range of 0.5 kHz to 80 kHz . The frequency of the IF signal is measured by counting the number of periods of the IF signal during a measurement time which is determined by bit 73 to bit 78 . The inverted STOP signal is available at pin 21 according to Table 29 on page 17 . The frequency of 10.25 MHz at pin 22 is used as a time reference.

Table 27. Search Stop Detector Measurement Time

| Time Window for Stop Signal | Bit 78 | Bit 77 | Bit 76 | Bit 75 | Bit 74 | Bit 73 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1 \times 3.1969 \mathrm{~ms}$ | 0 | 0 | 0 | 0 | 0 | 1 |
| $\ldots .$. |  |  |  |  |  |  |
| $63 \times 3.1969 \mathrm{~ms}$ | 1 | 1 | 1 | 1 | 1 | 1 |

Table 28. Search Stop Window

| Search Stop Window | Bit 87 | Bit 86 | Bit 85 |
| :---: | :---: | :---: | :---: |
| $\pm 0.5 \mathrm{kHz}$ | 0 | 0 | 0 |
| $\pm 1.1 \mathrm{kHz}$ | 0 | 0 | 1 |
| $\pm 2.3 \mathrm{kHz}$ | 0 | 1 | 0 |
| $\pm 4.8 \mathrm{kHz}$ | 0 | 1 | 1 |
| $\pm 10 \mathrm{kHz}$ | 1 | 0 | 0 |
| $\pm 20 \mathrm{kHz}$ | 1 | 0 | 1 |
| $\pm 40 \mathrm{kHz}$ | 1 | 1 | 0 |
| $\pm 80 \mathrm{kHz}$ | 1 | 1 | 1 |

Table 29. Signals Available at Digital Output Pin 21

| Bit 88 | Bit 92 | INT (Pin 21) |
| :---: | :---: | :---: |
| 0 | $0(\mathrm{AM})$ | 1 |
| 0 | $1(\mathrm{FM} / \mathrm{WB})$ | NOT MPINT |
| 1 | $0(\mathrm{AM})$ | NOT STOP |
| 1 | $1(\mathrm{FM} / \mathrm{WB})$ | NOT (STOP AND NOT MPINT) |

Note: MPINT = Multipath interrupt, Stop and MPINT signal are active low
Pin 35 (IFAGCH) is carried along with pin 36 (IFAGCL) to avoid crackles during a change of the search stop mode to the AM reception mode.

The deviation sensor is active in AM and FM/WB mode and measures the modulation of the signal. It is implemented as a peak detector of the low-pass-filtered MPX signal (see Figure 7). The output voltage at pin 31 is proportional to the frequency deviation in FM/WB or the modulation depth in AM respectively.

Figure 7. Deviation Sensor

## Deviation Sensor



## Adjacent Channel Sensor

The adjacent channel sensor is active in FM mode only and measures the field strength outside the reception band.

Figure 8. Adjacent Channel Sensor


MPINT and ADJAC Reset Bit 6 allows a resets of the multipath sensor and the adjacent channel sensor by connecting pin 10 and pin 40 internally to ground and so the external capacitors can be discharged very quickly.

Table 30. Multipath and Adjacent Channel Reset

| MPINT and Adjacent Channel (Pin 10 and Pin 40) | Bit 6 |
| :--- | :---: |
| Normal mode | 0 |
| Connection to ground | 1 |

## Multipath Sensor

The multipath sensor is active in FM mode only and measures the disturbance due to multipath reception. The multipath sensor detects drops in the field strength after the integrated band filter by calculating the difference between an averaged maximum field strength and the current field strength. The maximum depth of these drops is represented by the voltage of the peak detector at pin 40 (MULTIP). The level of this voltage represents the degree of disturbance in the received signal.

Figure 9. Multipath Sensor


A Multipath Noise Canceller (MNC) is implemented to reduce disturbance of the received signal in multipath reception conditions. If the difference between the momentary and the averaged field strength falls below a threshold adjustable by bit 81 to 84 (see Table 32), the MPX signal may be muted and this situation (MPINT) can be signalized at pin 21 (INT) according to Table 29 on page 17. Muting of the MPX signal during multipath disturbances can be activated be setting bit 8 .

Table 31. Multipath Noise Canceller

| Multipath Noise Canceller | Bit 8 |
| :---: | :---: |
| Active | 0 |
| Not active | 1 |

Table 32. Sensitivity of the MNC

| Sensitivity MNC (Threshold) | Bit 84 | Bit 83 | Bit 82 | Bit 81 |
| :---: | :---: | :---: | :---: | :---: |
| Off | 0 | 0 | 0 | 0 |
| Low | 0 | 0 | 0 | 1 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| $(-33 \mathrm{~dB})$ | 0 | 0 | 1 | 1 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| Normal (-14 dB) | 0 | 1 | 1 | 1 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| High $(-9 \mathrm{~dB})$ | 1 | 1 | 1 | 1 |

Note: $\quad$ Valid in FM or WB mode (bit $92=1$ )
The Multipath interrupt can also be switched on/off by bit 4.

Table 33. Multipath Interrupt (MPINT)

| MPINT (Pin 21) | Bit 4 |
| :--- | :---: |
| Off | 0 |
| On (MPINT active) | 1 |

AM Noise Blanker
The AM Noise Blanker of the ATR4258 can be activated by bit 5. The noise peak is detected in the field strength of the first IF and if the disturbance exceeds the level defined by the bits 85 to 87 , the signal is muted at the second IF.

Table 34. AM Noise Blanker Activation

| AM Noise Blanker | Bit 5 |
| :--- | :---: |
| Off | 0 |
| On | 1 |

Table 35. Sensitivity of AM Noise Blanker

| AM Noise Blanker Sensitivity | Bit 87 | Bit 86 | Bit 85 |
| :--- | :---: | :---: | :---: |
| Low | 0 | 0 | 0 |
| $\ldots .$. | $\ldots$ | $\ldots$ | $\ldots$ |
| Normal | 0 | 1 | 1 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| High | 1 | 1 | 1 |

3-wire Bus Description
The register settings of the ATR4258 are programmed by a 3-wire bus protocol. The bus protocol consists of separate commands. A defined number of bits are transmitted sequentially during each command.

One command is used to program all bits of one register. The different registers available (see Table 36 on page 22) are addressed by the length of the command (number of transmitted bits) and by three address bits that are unique for each register of a given length. 8-bit registers are programmed by 8-bit commands and 24-bit registers are programmed by 24-bit commands.

Each bus command starts with a rising edge on the enable line (EN) and ends with a falling edge on EN. EN has to be kept HIGH during the bus command.

The sequence of transmitted bits during one command starts with the LSB of the first byte and ends with the MSB of the last byte of the register addressed. The DATA is evaluated at the rising edges of CLK. The number of LOW to HIGH transitions on CLK during the HIGH period of EN is used to determine the length of the command.

The bus protocol and the register addressing of the ATR4258 are compatible to the addressing used in the U4256BM. That means both the ATR4258 and U4256BM can be operated on the same 3-wire bus as shown in the application circuit (Figure 20 on page 36).

Figure 10. Pulse Diagram
8-bit command


Figure 11. Bus Timing


## Data Transfer

Table 36. Control Registers

| A24_100 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MSB |  |  | BYTE 3 |  | LSB |  |  | MSB | BYTE 2 |  |  |  |  | LSB |  | MSB |  | BYTE 1 |  |  |  | LSB |  |
| ADDR. |  |  | Demodulator AM/FM/WB |  | Gain FM IF amplifier |  |  | Search | Width of window |  |  | AM OSC divider/multipath sensitivity |  |  |  | Field strength | BW/ <br> MPX/ <br> LPF/ | Time window stop signal |  |  |  |  |  |
| 1 | 0 | 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | B93 | B92 | B91 | B90 | B89 | B88 | B87 | B86 | B85 | B84 | B83 | B82 | B81 | B80 | B79 | B78 | B77 | B76 | B75 | B74 | B73 |



A24_111


| A8_100 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MSB |  |  | BYTE 1 |  |  | LSB |  |
| ADDR. |  |  | Test mode | MP | Mute (pin 11) | Reset MP/ ADJ | Noiseblanker |
| 1 | 0 | 0 | 0 |  |  |  |  |
|  |  |  | B9 | B8 | B7 | B6 | B5 |


| A8_101 |  |  |  |  |  |  |  |
| :--- | :--- | :--- | ---: | ---: | ---: | ---: | ---: |
| MSB |  |  |  |  |  |  |  |
| ADDR. |  | MP <br> INT | Band-path filter <br> Band width |  |  |  |  |
| 1 | 0 | 1 |  |  |  |  |  |
|  |  |  | B4 | B3 | B2 | B1 | B0 |

## Absolute Maximum Ratings

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress rating only and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.
All voltages are referred to GND (pin 25)

| Parameters | Symbol | Value | Unit |
| :--- | :---: | :---: | :---: |
| Supply voltage, pin 42 | $\mathrm{V}_{\mathrm{S}}$ | 10 | V |
| Power dissipation | $\mathrm{P}_{\text {tot }}$ | 1000 | mW |
| Junction temperature | $\mathrm{T}_{\mathrm{j}}$ | 150 | ${ }^{\circ} \mathrm{C}$ |
| Ambient temperature range | $\mathrm{T}_{\mathrm{amb}}$ | -40 to +85 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature range | $\mathrm{T}_{\text {stg }}$ | -50 to +150 | ${ }^{\circ} \mathrm{C}$ |

## Thermal Resistance

| Parameters | Symbol | Value | Unit |
| :--- | :---: | :---: | :---: |
| Junction ambient, soldered to PCB | $\mathrm{R}_{\mathrm{thJA}}$ | 60 | K/W |

## Operating Range

All voltages are referred to GND (pin 25)

| Parameters | Symbol | Min. | Typ. | Max. | Unit |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Supply voltage range, pin 42 | $\mathrm{V}_{\mathrm{S}}$ | 8.0 | 8.5 | 10 | V |
| Ambient temperature | $\mathrm{T}_{\mathrm{amb}}$ | -40 |  | +85 | ${ }^{\circ} \mathrm{C}$ |

## Electrical Characteristics

Test conditions (unless otherwise specified): $\mathrm{V}_{\mathrm{S}}=8.5 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| No. | Parameters | Test Conditions | Pin | Symbol | Min. | Typ. | Max. | Unit | Type* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Power Supply |  |  |  |  |  |  |  |  |
| 1.1 | Supply voltage |  | 42 | $\mathrm{V}_{\text {S }}$ | 8.0 | 8.5 | 10 | V | C |
| 1.2 | Supply current | Standby mode (bit $92=0$, bit $93=0$ ) | 42 | $I_{\text {Stby }}$ |  | 35 | 45 | mA | A |
| 1.3 | Supply current | Other operation modes | 42 | $I_{\text {S }}$ |  | 50 | 65 | mA | A |
| 2 | VCO (Bit $52=0$, Bit $30=1$ ) |  |  |  |  |  |  |  |  |
| 2.1 | Frequency range |  |  | fvCo | 70 |  | 260 | MHz | D |
| 2.2 | DC bias voltage |  | 13 |  | 3.4 | 3.7 | 4.0 | V | A |
| 2.3 | Buffer output voltage | $\mathrm{f}_{\text {osc }}=120 \mathrm{MHz}$ | 16 |  |  | 250 |  | mVrms | C |
| 2.4 | Buffer output resistance |  | 16 |  |  | 70 |  | $\Omega$ | D |
| 2.5 | Buffer output DC voltage |  | 16 |  | 3.8 | 4.1 | 4.4 | V | A |
| 3 | FM RF-AGC |  |  |  |  |  |  |  |  |
| 3.1 | Saturation voltage | No input signal | 5 |  | 8.3 |  |  | V | A |
| 3.2 | Saturation voltage | No input signal | 5 |  | $\mathrm{V}_{\mathrm{S}}-0.2$ |  |  | V | B |

${ }^{*}$ ) Type means: $A=100 \%$ tested, $B=100 \%$ correlation tested, $C=$ Characterized on samples, $D=$ Design parameter

Electrical Characteristics (Continued)
Test conditions (unless otherwise specified): $\mathrm{V}_{\mathrm{S}}=8.5 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| No. | Parameters | Test Conditions | Pin | Symbol | Min. | Typ. | Max. | Unit | Type* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3.3 | Threshold level | In-band signal | 30 |  |  | 115 |  | $\mathrm{dB} \mu \mathrm{V}$ | C |
| 3.4 | Maximum threshold level | Out-of-band signal ( 110 MHz ), bit $64,65=0$ | 1 |  | 100 | 103 | 106 | $\mathrm{dB} \mu \mathrm{V}$ | B |
| 4 | AM RF-AGC, AM Mode (Bit 92 = 0, Bit 93 = 1) |  |  |  |  |  |  |  |  |
| 4.1 | Saturation voltage | No input signal | 7 |  | 8.3 |  |  | V | C |
| 4.2 | Saturation voltage | No input signal | 7 |  | $\mathrm{V}_{\mathrm{S}}-0.2$ |  |  | V | C |
| 4.3 | Output voltage for minimum gain | Bit $92=1$ | 7 |  | 6.5 | 6.8 | 7.1 | V | C |
| 4.4 | Output voltage for minimum gain | Bit $92=1$ | 7 |  |  | $\begin{gathered} \mathrm{V}_{\mathrm{S}}- \\ 1.7 \end{gathered}$ |  | V | C |
| 4.5 | Maximum control voltage | No signal | 6 |  | 6.5 | 7.0 | 7.5 | V | A |
| 4.6 | Maximum control voltage | No signal | 6 |  |  | $V_{S}-1.5$ |  | V | B |
| 4.7 | Minimum control voltage | AGC active | 6 |  |  | 0.2 | 0.8 | V | A |
| 4.8 | Maximum threshold level | Bits 64, $65=1$ | 41 |  | 97 | 99 | 102 | $\mathrm{dB} \mu \mathrm{V}$ | A |
| 5 | AM Mixer, AM Mode (Bit $92=0$, Bit $93=1$ ) |  |  |  |  |  |  |  |  |
| 5.1 | Supply current | Sum of current in pins 43, 44 | 43, 44 |  | 14 | 16 | 20 | mA | A |
| 5.2 | Conversion conductance |  | $\begin{aligned} & \hline 3,41 \\ & 43,44 \end{aligned}$ |  |  | 4.1 |  | mS | D |
| 5.3 | $3^{\text {rd }}$-order input intercept point | Pin 3 AC-grounded | 41 | $\mathrm{IP}^{\text {AMmix }}$ |  | 132 |  | $\mathrm{dB} \mu \mathrm{V}$ | C |
| 5.4 | Noise figure (SSB) | Generator resistance $2.5 \mathrm{k} \Omega(\operatorname{pin} 41)$ | 43, 44 | $N F_{\text {AMmix }}$ |  | 12 |  | dB | C |
| 5.5 | Input bias DC voltage |  | 3,41 |  | 2.45 | 2.8 | 3.1 | V | A |
| 5.6 | Input resistance | Single-ended, pin 39 AC-grounded | 3,41 |  |  | 13 |  | $\mathrm{k} \Omega$ | D |
| 5.7 | Input capacitance |  | 3,41 |  |  |  | 3 | pF | D |
| 5.8 | Maximum output voltage | Differential | 43, 44 |  | 12 |  |  | Vpp | D |
| 5.9 | Output resistance |  | 43, 44 |  | 100 |  |  | $\mathrm{k} \Omega$ | D |
| 6 | FM Mixer (FM Mode (Bit $92=1$, Bit $93=0$ ) |  |  |  |  |  |  |  |  |
| 6.1 | Supply current | Sum of current in pins 43, 44 | 43, 44 |  | 12 | 15 | 20 | mA | A |
| 6.2 | Conversion conductance |  | $\begin{gathered} 1,2, \\ 43,44 \end{gathered}$ |  |  | 7 |  | mS | D |
| 6.3 | $3^{\text {rd }}$-order intercept point |  | 1, 2 | $I P 3_{\text {FMmix }}$ |  | 125 |  | $\mathrm{dB} \mu \mathrm{V}$ | C |
| 6.4 | Noise figure (DSB) | Generator resistance $200 \Omega$ | 43, 44 | $\mathrm{NF}_{\text {FMmix }}$ |  | 10 |  | dB | C |

${ }^{*}$ ) Type means: $A=100 \%$ tested, $B=100 \%$ correlation tested, $C=$ Characterized on samples, $D=$ Design parameter

## Electrical Characteristics (Continued)

Test conditions (unless otherwise specified): $\mathrm{V}_{\mathrm{S}}=8.5 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| No. | Parameters | Test Conditions | Pin | Symbol | Min. | Typ. | Max. | Unit | Type* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6.5 | Input resistance |  | 1, 2 |  |  | 1.6 |  | k $\Omega$ | D |
| 6.6 | Input capacitance | Pin 2 AC-grounded | 1 |  |  | 5 |  | pF | D |
| 6.7 | Maximum differential output voltage | $\mathrm{V}_{\mathrm{S}}=8.5 \mathrm{~V}$ | 43, 44 |  | 12 |  |  | Vpp | D |
| 6.8 | Output resistance |  | 43, 44 |  | 100 |  |  | k $\Omega$ | D |
| 7 | $1^{\text {st }}$ IF FM Amplifier, FM Mode (Bit $92=1$, Bit $93=0$ ) |  |  |  |  |  |  |  |  |
| 7.1 | Minimum voltage gain | Bits 89, 90, $91=0$ | 38, 30 |  | 19 | 21 | 23 | dB | B |
| 7.2 | Temperature coefficient of gain | Bit $66=0$ |  | TK ${ }_{\text {min }}$ |  | 0.039 |  | dB/K | D |
| 7.3 | Temperature coefficient of gain | Bit $66=1$ |  | TK ${ }_{\text {max }}$ |  | 0.044 |  | dB/K | D |
| 7.4 | Input resistance | Pin 39 AC-grounded | 38 |  | 270 | 330 | 400 | $\Omega$ | D |
| 7.5 | Input capacitance | Pin 39 AC-grounded | 38 |  |  | 5 |  | pF | D |
| 7.6 | Output resistance |  | 30 |  | 270 | 330 | 400 | $\Omega$ | D |
| 8 | $1^{\text {st }}$ IF AM Amplifier, AM Mode (Bit $92=0$, Bit $93=1$ ) |  |  |  |  |  |  |  |  |
| 8.1 | Maximum voltage gain | $330 \Omega$ load at pin 30 | 30, 33 |  |  | 16 |  | dB | D |
| 8.2 | Gain control range |  |  |  |  | 26 |  | dB | D |
| 8.3 | Noise figure | Generator resistance $2.5 \mathrm{k} \Omega$ |  | $\mathrm{NF}_{\text {IFAM }}$ |  | 17 |  | dB | D |
| 8.4 | Input resistance |  | 33 |  | 10 |  |  | $\mathrm{k} \Omega$ | D |
| 8.5 | Input capacitance | Pin 39 AC-grounded | 33 |  |  | 1 |  | pF | D |
| 8.6 | Output resistance |  | 30 |  | 270 | 330 | 400 | $\Omega$ | D |
| 9 | $2^{\text {nd }}$ Mixer |  |  |  |  |  |  |  |  |
| 9.1 | FM supply current | Bit $92=1$, Bit $93=0$ | 23, 24 |  | 10 | 12 | 16 | mA | A |
| 9.2 | AM/WB supply current | Bit $92=0$, Bit $93=1$ | 23, 24 |  | 7 | 8 | 10 | mA | A |
| 9.3 | Conversion conductance |  | $\begin{gathered} 26,23, \\ 24 \end{gathered}$ |  |  | 2 |  | mS | D |
| 9.4 | Noise figure (SSB) | Generator resistance $330 \Omega$ (pin 26) | 23, 24 | $N F_{\text {Mix } 2}$ |  | 23 |  | dB | C |
| 9.5 | $3^{\text {rd }}$-order input intercept point |  | 26 | $1 \mathrm{P} 3_{\text {Mix2 }}$ |  | 132 |  | $\mathrm{dB} \mu \mathrm{V}$ | C |
| 9.6 | AM/WB output resistance | Bit $92=0$, Bit 93 = 1 | 23, 24 |  | 100 |  |  | $\mathrm{k} \Omega$ | D |
| 9.7 | Maximum differential output voltage AM/WB | $\mathrm{V}_{\mathrm{S}}=8.5 \mathrm{~V}$ | 23, 24 |  | 12 |  |  | Vpp | D |
| 9.8 | Maximum differential output voltage FM |  | 23, 24 |  | 1 |  |  | Vpp | D |
| 9.9 | Input resistance |  | 26 |  | 270 | 330 | 400 | $\Omega$ | D |
| 9.10 | LO input voltage |  | 22 |  | 80 |  | 500 | mVpp | D |

${ }^{*}$ ) Type means: $A=100 \%$ tested, $B=100 \%$ correlation tested, $C=$ Characterized on samples, $D=$ Design parameter

Electrical Characteristics (Continued)
Test conditions (unless otherwise specified): $\mathrm{V}_{\mathrm{S}}=8.5 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| No. | Parameters | Test Conditions | Pin | Symbol | Min. | Typ. | Max. | Unit | Type* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9.11 | LO input resistance |  | 22 |  |  | 1 |  | k $\Omega$ | D |
| 9.12 | LO input bias voltage |  | 22 |  | 2.8 | 3.0 | 3.2 | V | A |
| 10 | $2^{\text {nd }}$ IF Amplifier (Bit $55=0$ ) |  |  |  |  |  |  |  |  |
| 10.1 | Input resistance | Pin 27 AC-grounded | 28 |  |  | 3 |  | k $\Omega$ | D |
| 10.2 | Voltage gain | AM/WB mode <br> (Bit $93=1$ ) <br> Pin 281 mVrms | 28, 20 |  | 42 | 45 | 48 | dB | A |
| 10.3 | Gain control range | AM/WB mode $\text { (Bit } 93 \text { = 1) }$ |  |  |  | 47 |  | dB | D |
| 10.4 | DC output voltage |  | 20 |  | 3.4 | 3.7 | 4.0 | V | A |
| 10.5 | AC output voltage | Unmodulated signal, $82 \mathrm{~dB} \mu \mathrm{~V}$ at pin 1 (IF AGC active) Bit $93=1$ | 20 |  | 150 | 180 | 230 | mVrms | A |
| 10.6 | Output impedance | Small signal | 20 |  |  | 70 |  | $\Omega$ | D |
| 11 | FM Demodulator Integrated Band-filter, FM Mode (Bit 92 = 1, Bit 93 = 0), BW Setting ${ }^{\text {nd }}$ IF Filter = 120 kHz |  |  |  |  |  |  |  |  |
| 11.1 | AC output voltage | $\begin{aligned} & \text { Deviation }= \pm 75 \mathrm{kHz} \\ & \mathrm{f}_{\text {mod }}=1 \mathrm{kHz} \end{aligned}$ | 11 |  | 420 | 480 | 540 | mVrms | B |
| 11.2 | Stereo roll-off | $\begin{aligned} & \text { Deviation }= \pm 75 \mathrm{kHz} \\ & \mathrm{f}_{\text {mod }}=38 \mathrm{kHz} \\ & \text { (reference: } 1 \mathrm{kHz} \text { ) } \end{aligned}$ | 11 |  |  | -2.0 |  | dB | D |
| 11.3 | Total harmonic distortion | $\begin{aligned} & \text { Deviation }= \pm 75 \mathrm{kHz}, \\ & \mathrm{f}_{\text {mod }}=1 \mathrm{kHz} \end{aligned}$ | 11 | THD FM |  | 0.4 | 0.7 | \% | A |
| 11.4 | Maximum signal-tonoise ratio | Dev. $= \pm 22.5 \mathrm{kHz}$, $\mathrm{f}_{\text {mod }}=1 \mathrm{kHz}, 50 \mu \mathrm{~s}$ de-emphase, signal input at 450 kHz | 11 | $(\mathrm{S} / \mathrm{N})_{\mathrm{FM}}$ |  | 65 |  | dB | C |
| 12 | Soft Mute, FM Mode (Bit $92=1$, Bit $93=0$, Bit $80=0$ ) |  |  |  |  |  |  |  |  |
| 12.1 | Mute gain | $\begin{aligned} & \text { Bit } 67=0, \\ & V(\operatorname{pin} 34)=2 \vee \end{aligned}$ | 11 |  | -28 | -26 | -24 | dB | A |
| 12.2 | Mute gain | $\begin{aligned} & \text { Bit } 67=1, \\ & V(\operatorname{pin} 34)=2 V \end{aligned}$ | 11 |  | -24 | -22 | -20 | dB | A |
| 13 | AM Demodulator, AM Mode (Bit $92=0$, Bit $93=1$ ) |  |  |  |  |  |  |  |  |
| 13.1 | AC output voltage | Modulation depth = $30 \%, \mathrm{f}_{\mathrm{mod}}=1 \mathrm{kHz}$ | 11 |  | 135 | 150 | 170 | mVrms | A |
| 13.2 | Total harmonic distortion | Modulation depth $=$ $80 \%, \mathrm{f}_{\text {mod }}=1 \mathrm{kHz}$ <br> $\mathrm{V}($ pin 35$)=$ const. | 11 | THD ${ }_{\text {AM }}$ |  | 0.6 | 2 | \% | A |
| 13.3 | Maximum signal-to-noise ratio | Modulation depth $=$ $30 \%, f_{\text {mod }}=1 \mathrm{kHz}$ $74 \mathrm{~dB} \mu \mathrm{~V}$ at pin 41 | 11 | $(\mathrm{S} / \mathrm{N})_{\mathrm{Am}}$ |  | 54 |  | dB | C |
| 14 | MPX Output |  |  |  |  |  |  |  |  |
| 14.1 | DC output voltage | Bit $7=1$ | 11 |  | 2.1 | 2.3 | 2.5 | V | A |

${ }^{*}$ ) Type means: $A=100 \%$ tested, $B=100 \%$ correlation tested, $C=$ Characterized on samples, $D=$ Design parameter

## Electrical Characteristics (Continued)

Test conditions (unless otherwise specified): $\mathrm{V}_{\mathrm{S}}=8.5 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| No. | Parameters | Test Conditions | Pin | Symbol | Min. | Typ. | Max. | Unit | Type* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14.2 | Mute gain | Bit $7=1$, <br> FM dev. $= \pm 75 \mathrm{kHz}$, $\mathrm{f}_{\text {mod }}=1 \mathrm{kHz}$ | 11 |  |  | -65 | -50 | dB | A |
| 14.3 | Output resistance | Small signal | 11 |  |  | 60 |  | $\Omega$ | D |
| 15 | Search Stop Detector, INT Output |  |  |  |  |  |  |  |  |
| 15.1 | LOW saturation voltage |  | 21 |  |  | 0 | 0.5 | V | A |
| 15.2 | LOW output resistance |  | 21 |  |  | 0.3 |  | $\mathrm{k} \Omega$ | D |
| 15.3 | HIGH saturation voltage |  | 21 |  | 4.5 | 4.8 | 5.25 | V | A |
| 15.4 | HIGH output resistance |  | 21 |  |  | 1 |  | $\mathrm{k} \Omega$ | D |
| 16 | Deviation Sensor, FM Mode (Bit $92=1$, Bit $93=0$ ) |  |  |  |  |  |  |  |  |
| 16.1 | Offset voltage | FM dev. $= \pm 0 \mathrm{kHz}$ FM demodulator adjusted | 31 |  |  | 0.2 |  | V | C |
| 16.2 | Output voltage | $\begin{aligned} & \text { FM dev. }= \pm 75 \mathrm{kHz}, \\ & \mathrm{f}_{\text {mod }}=1 \mathrm{kHz} \end{aligned}$ | 31 |  | 1.7 | 2.0 | 2.5 | V | C |
| 17 | Field Strength Sensor, FM Mode (Bit $92=1$, Bit $93=0$, Bit 89 to $91=0$, Bit $80=0$, Bit 18 to $21=0$ ) |  |  |  |  |  |  |  |  |
| 17.1 | Output voltage | $60 \mathrm{~dB} \mu \mathrm{~V}$ at pin 33 | 9 |  | 0.8 | 1.3 | 1.8 | V | A |
| 17.2 | Output voltage | Unmodulated signal $100 \mathrm{~dB} \mu \mathrm{~V}$ at pin 33 | 9 |  | 2.8 | 3.4 | 3.9 | V | A |
|  | Field Strength Sensor, AM Mode (Bit $92=0$, Bit $93=1$, Bit $80=1$, Bit 18 to $21=0$ ) |  |  |  |  |  |  |  |  |
| 17.3 | Output voltage LOW field strength | $60 \mathrm{~dB} \mathrm{\mu} \mathrm{~V}$ at pin 28 | 9 |  | 1.5 | 1.8 | 2.1 | V | A |
| 17.4 | Output voltage HIGH field strength | $94 \mathrm{~dB} \mu \mathrm{~V}$ at pin 28 | 9 |  | 3.0 | 3.3 | 3.6 | V | A |
| 18 | Multipath Sensor, FM Mode (Bit $92=1$, Bit 93 = 0) |  |  |  |  |  |  |  |  |
| 18.1 | Offset voltage | Unmodulated signal, $60 \mathrm{~dB} \mu \mathrm{~V}$ at pin 1 | 40 |  |  | 0 | 200 | mV | A |
| 18.2 | Output voltage | AM modulation depth $\begin{aligned} & =60 \%, \\ & \mathrm{f}_{\text {mod }}=20 \mathrm{kHz}, \end{aligned}$ $60 \mathrm{~dB} \mu \mathrm{~V} \text { at pin } 1$ | 40 |  | 1.5 | 1.9 | 2.4 | V | A |

[^0]
## Electrical Characteristics (Continued)

Test conditions (unless otherwise specified): $\mathrm{V}_{\mathrm{S}}=8.5 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| No. | Parameters | Test Conditions | Pin | Symbol | Min. | Typ. | Max. | Unit | Type* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | Adjacent Channel Sensor, FM Mode (Bit $92=1$, Bit $93=0$ ), Bit 4 = 0 (Default BW Setting) |  |  |  |  |  |  |  |  |
| 19.1 | Offset voltage | Unmodulated signal | 10 |  |  | 200 |  | mV | C |
| $\begin{aligned} & 19.2 \\ & 19.3 \end{aligned}$ | Output voltage | AM mod. 10\% $\mathrm{f}_{\text {mod }}=100 \mathrm{kHz}$ AM mod. 60\% $\mathrm{f}_{\text {mod }}=100 \mathrm{kHz}$ | 10 |  | 1.2 | $\begin{aligned} & 0.3 \\ & 1.9 \end{aligned}$ | $\begin{aligned} & 0.6 \\ & 2.5 \end{aligned}$ | V | A |
| 20 | 3-wire Bus |  |  |  |  |  |  |  |  |
| 20.1 | Input voltage LOW |  | $\begin{gathered} 17,18, \\ 19 \end{gathered}$ |  |  |  | 0.8 | V | D |
| 20.2 | Input voltage HIGH |  | $\begin{gathered} 17,18 \\ 19 \end{gathered}$ |  | 2.7 |  |  | V | D |
| 20.3 | Leakage current | $\mathrm{V}=0 \mathrm{~V}, 5 \mathrm{~V}$ | $\begin{gathered} 17,18, \\ 19 \end{gathered}$ |  |  |  | 10 | $\mu \mathrm{A}$ | D |
| 20.4 | Clock frequency |  | 18 |  |  |  | 1.0 | MHz | D |
| 20.5 | Period of CLK HIGH LOW |  |  | $\begin{aligned} & \mathrm{t}_{\mathrm{H}} \\ & \mathrm{t}_{\mathrm{L}} \end{aligned}$ | $\begin{aligned} & 250 \\ & 250 \end{aligned}$ |  |  | $\begin{aligned} & \mathrm{ns} \\ & \mathrm{~ns} \end{aligned}$ | D |
| 20.6 | Rise time EN, DATA, CLK |  |  | $\mathrm{t}_{\mathrm{r}}$ |  |  | 400 | ns | D |
| 20.7 | Fall time <br> EN, DATA, CLK |  |  | $t_{\text {f }}$ |  |  | 100 | ns | D |
| 20.8 | Set-up time |  |  | $\mathrm{t}_{\text {s }}$ | 100 |  |  | ns | D |
| 20.9 | Hold time EN |  |  | $\mathrm{t}_{\text {HEN }}$ | 250 |  |  | ns | D |
| 20.10 | Hold time DATA |  |  | $\mathrm{t}_{\text {HDA }}$ | 0 |  |  | ns | D |
| 21 | Internally Generated Reference Voltages |  |  |  |  |  |  |  |  |
| 21.1 | Output voltage |  | 12 |  | 5.5 | 5.7 | 6.0 | V | A |
| 21.2 | Output voltage |  | 29 |  |  | 3.0 |  | V | D |
| 21.3 | Output voltage |  | 27 |  |  | 3.0 |  | V | D |
| 21.4 | Output voltage |  | 39 |  |  | 3.0 |  | V | D |

*) Type means: $A=100 \%$ tested, $B=100 \%$ correlation tested, $C=$ Characterized on samples, $D=$ Design parameter

## Application Information

AM Prescaler (Divider) Settings

The AM mixer is used for up conversion of the AM reception frequency to the IF frequency. Therefore an AM prescaler is implemented to generate the necessary LO from the VCO frequency. For the reception of the AM band different prescaler (divider) settings are possible.

Table 37 gives an example for the AM prescaler (divider) settings and the reception frequencies.
e.g.,

$$
\begin{aligned}
& \mathrm{f}_{\mathrm{VCO}}=98.2 \mathrm{MHz} \ldots 124 \mathrm{MHz} \\
& \mathrm{f}_{\mathrm{IF}}=10.7 \mathrm{MHz} \\
& \mathrm{f}_{\text {rec }}=\left(\frac{\mathrm{f}_{\mathrm{Vco}}}{\text { AM Prescaler }}\right)-\mathrm{f}_{\mathrm{IF}}
\end{aligned}
$$

Table 37. AM Prescaler (Divider) Settings and Reception Frequencies

| Divider (AM Prescaler) | Minimum Reception Frequency <br> $[\mathbf{M H z}]$ | Maximum Reception Frequency <br> $[\mathbf{M H z}]$ |
| :---: | :---: | :---: |
| divide by 2 | 38.4 | 51.3 |
| divide by 3 | 20.033 | 30.633 |
| divide by 4 | 13.85 | 20.3 |
| divide by 5 | 8.94 | 14.1 |
| divide by 6 | 5.667 | 9.967 |
| divide by 7 | 3.329 | 7.014 |
| divide by 8 | 1.575 | 4.8 |
| divide by 9 | 0.211 | 3.078 |
| divide by 10 | 0 | 1.7 |

Note: $\quad$ Prescaler VCO Divider $=1$ in this example.

Local Oscillator and AM Prescaler Settings

Table 38 gives an example for the VCO prescaler divider and AM prescaler divider settings and the reception frequencies.
e.g.,

$$
\begin{aligned}
& \mathrm{f}_{\mathrm{VCO}}=195.9 \mathrm{MHz} \ldots 237.9 \mathrm{MHz} \\
& \mathrm{f}_{\mathrm{IF}}=+10.7 \mathrm{MHz} \text { or }-10.7 \mathrm{MHz} \\
& \mathrm{f}_{\mathrm{VCO}}=\left(\mathrm{f}_{\mathrm{rec}}+\mathrm{f}_{\mathrm{IF}}\right) \times \mathrm{VCO} \text { Prescaler } \times \text { AM Prescaler }
\end{aligned}
$$

Table 38. VCO and AM Prescaler (Divider) Settings and Reception Frequencies

| Band | Prescaler <br> VCO | IF [MHz] | Minimum Reception <br> Frequency [MHz] | Maximum Reception <br> Frequency [MHz] | Minimum VCO <br> Frequency | Maximum VCO <br> Frequency | AM <br> Prescaler |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FM | 2 | +10.7 | 87.5 | 108 | 196.4 | 237.4 | - |
| WB | 1.5 | -10.7 | 162.4 | 162.55 | 227.55 | 227.775 | - |
| JPN | 3 | -10.7 | 76 | 90 | 195.9 | 237.9 | - |
| LW/MW | 2 | +10.7 | 0.15 | 1.605 | 195.3 | 221.49 | 9 |
| 16 m | 1 | +10.7 | 17.5 | 17.9 | 225.6 | 228.8 | 8 |
| 120 m | 2 | +10.7 | 2.3 | 2.5 | 208 | 211.2 | 8 |

## U4256 N- and R-divider

Calculation

## AM Mode

$$
\begin{aligned}
& N=\frac{f_{V C O}}{\text { VCO-divider } \times \text { AM Prescaler } \times f_{\text {step }}} \\
& f_{\text {rec }}=\left(\frac{f_{V C O}}{\text { VCO-divider } \times \text { AM Prescaler }}\right)-f_{I F}
\end{aligned}
$$

FM/WB Mode

$$
\begin{aligned}
& \mathrm{N}=\frac{\mathrm{f}_{\mathrm{VCO}}}{\mathrm{VCO} \text {-divider } \times \mathrm{f}_{\text {step }}} \\
& \mathrm{f}_{\text {rec }}=\left(\frac{\mathrm{f}_{\mathrm{VCO}}}{\mathrm{VCO} \text {-divider }}\right)-\mathrm{f}_{\mathrm{lF}}
\end{aligned}
$$

## All Modes

$$
\mathrm{R}=\frac{\mathrm{f}_{\text {ref }}}{\mathrm{f}_{\text {step }}}
$$

$\mathrm{f}_{\text {ref }}=$ reference oscillator frequency (e.g. 10.25 MHz)
$\mathrm{f}_{\mathrm{vco}}=\mathrm{VCO}$ frequency
$\mathrm{f}_{\text {rec }}=$ reception frequency
$\mathrm{f}_{\text {step }}=$ step frequency (of the PLL)

The following data was measured with the application board (see Figure 20).
In the measurement setup, a $50 \Omega$ generator is terminated by $50 \Omega$ and connected to the antenna input by a $50 \Omega$ series resistor to achieve $75 \Omega$ termination at the antenna input. The generator level specified is the output voltage of this $50 \Omega$ generator at $50 \Omega$ load. If the application board is replaced by a $75 \Omega$ resistor, the voltage at this resistor is 6 dB below the specified voltage level of the $50 \Omega$ generator.

Figure 12. FM Demodulator


Note: Integrated band-filter BW setting: 120 kHz (bits 0 to $2=0$, bit $3=1$ ); 1 kHz modulation frequency; $50 \mu \mathrm{~s}$ de-emphasis (THD)

Figure 13. Multipath Sensor


Note: $\quad \mathrm{AM}$ modulation frequency 20 kHz ; generator level $40 \mathrm{~dB} \mu \mathrm{~V}$

Figure 14. Multipath Sensor Frequency Response


Note: Generator level $40 \mathrm{~dB} \mu \mathrm{~V}$
Figure 15. Deviation Sensor


Note: FM modulation frequency: 1 kHz ; BW setting $2^{\text {nd }}$ IF filter $=120 \mathrm{kHz}$; demodulator fine tuning (bit $53=0$ )
The center frequency of the integrated band filter has to adjusted (e.g., IF center frequency $=462.50 \mathrm{kHz}$ ).

Figure 16. Deviation Sensor Frequency Response


Note: FM frequency deviation: 22.5 kHz
Figure 17. FM Input Level Sweep


Fieldstrength Sensor Output Voltage [V]

Note: Soft mute threshold bits $68,69=0$, bit $70=1$; soft mute gain bit $67=0$ gain FM IF amplifier bit 89 to $91=1$

Figure 18. Selectivity


Note: Integrated bandfilter BW setting: 120 kHz
Desired signal level adjusted to $40 \mathrm{~dB} \mathrm{S/N}$ without undesired signal Undesired signal level adjusted to 26 dB S/N

Figure 19. Test Circuit


Figure 20. Application Circuit


Ordering Information

| Extended Type Number | Package | Remarks |
| :--- | :---: | :--- |
| ATR4258-ILSH | SSO44 | Tube, lead-free |
| ATR4258-ILQH | SSO44 | Taped and reeled, lead-free |

Package Information


## Atmel Corporation

2325 Orchard Parkway
San Jose, CA 95131, USA
Tel: 1(408) 441-0311
Fax: 1(408) 487-2600

## Regional Headquarters

## Europe

Atmel Sarl
Route des Arsenaux 41
Case Postale 80
CH-1705 Fribourg
Switzerland
Tel: (41) 26-426-5555
Fax: (41) 26-426-5500
Asia
Room 1219
Chinachem Golden Plaza
77 Mody Road Tsimshatsui
East Kowloon
Hong Kong
Tel: (852) 2721-9778
Fax: (852) 2722-1369
Japan
9F, Tonetsu Shinkawa Bldg.
1-24-8 Shinkawa
Chuo-ku, Tokyo 104-0033
Japan
Tel: (81) 3-3523-3551
Fax: (81) 3-3523-7581

## Atmel Operations

Memory<br>2325 Orchard Parkway<br>San Jose, CA 95131, USA<br>Tel: 1(408) 441-0311<br>Fax: 1(408) 436-4314

## Microcontrollers

2325 Orchard Parkway
San Jose, CA 95131, USA
Tel: 1(408) 441-0311
Fax: 1(408) 436-4314
La Chantrerie
BP 70602
44306 Nantes Cedex 3, France
Tel: (33) 2-40-18-18-18
Fax: (33) 2-40-18-19-60
ASIC/ASSP/Smart Cards
Zone Industrielle
13106 Rousset Cedex, France
Tel: (33) 4-42-53-60-00
Fax: (33) 4-42-53-60-01
1150 East Cheyenne Mtn. Blvd.
Colorado Springs, CO 80906, USA
Tel: 1(719) 576-3300
Fax: 1(719) 540-1759
Scottish Enterprise Technology Park
Maxwell Building
East Kilbride G75 0QR, Scotland
Tel: (44) 1355-803-000
Fax: (44) 1355-242-743

## RF/Automotive

## Theresienstrasse 2

Postfach 3535
74025 Heilbronn, Germany
Tel: (49) 71-31-67-0
Fax: (49) 71-31-67-2340
1150 East Cheyenne Mtn. Blvd.
Colorado Springs, CO 80906, USA
Tel: 1(719) 576-3300
Fax: 1(719) 540-1759
Biometrics/Imaging/Hi-Rel MPU/
High Speed Converters/RF Datacom Avenue de Rochepleine
BP 123
38521 Saint-Egreve Cedex, France
Tel: (33) 4-76-58-30-00
Fax: (33) 4-76-58-34-80

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[^0]:    *) Type means: $A=100 \%$ tested, $B=100 \%$ correlation tested, $C=$ Characterized on samples, $D=$ Design parameter

